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Detecting quasiperiodic structures with double diffraction

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Abstract – We study interference patterns of double-diffraction systems with quasiperiodic structures. A quasiperiodic linear array of scatterers converts single delta pulses into a sequence of quasiperiodic pulses. This pulse train is diffracted from a second set of scatterers. We find that the interference pattern after the second diffraction has a pronounced peak if both sets of scatterers have similar quasiperiodic structures. We show that this method can be used for identifying the Fibonacci chain and related quasiperiodic sequences, if the number of scatterers in the first set is at least twice as large as the number of scatterers in the second set, and if the distances among the two sets of scatterers and the detector are all large compared to the size of the sets. This method may provide a methodology for identifying the structure of quasicrystals and quasiperiodic layered materials with a large signal-to-noise ratio.

Introduction. – Since the discovery of quasicrystals in 1984 [1], their diffraction patterns have been extensively studied both theoretically [2,3] and experimentally [4–6]. Most of this work is based on hyperspace crystallography [7]. However, standard X-ray diffraction experiments do not provide a unique structure, due to the local isomorphic nature of a quasilattice [8]. A similar ambiguity in identifying nonlinear dynamical systems can be resolved with aperiodic forcing functions [9–16]. More recent work shows that by using quasiperiodic pulse trains, it is possible to obtain diffraction patterns with only one major diffraction peak [17]. But the production of such a quasiperiodic pulse train is still an open question. Can the quasiperiodic pulse be produced with a second set of scatterers? If so, how closely do the structural parameters of the two sets of scatterers have to match to produce a diffraction peak and what is the minimum size of the second set of scatterers? How does the geometry of the setup influence the signal-to-noise ratio?

In this paper, we discuss a double-diffraction technique, where a set of quasiperiodic scatterers creates a quasiperiodic pulse train, which is then used to identify the structure of a second set of quasiperiodic scatterers. The first set of point scatterers is called the source, the second set of scatterers is called the target. In a double-diffraction system a single-pulse plane wave is diffracted from the source. The diffracted wave forms a quasiperiodic pulse train in the far field. A screen prevents the quasiperiodic pulse train from reaching the detector. The pulse train is then diffracted from the target. After the quasiperiodic pulse train wave is diffracted from the target, it creates an interference pattern on the detector screen. We assume that there is a set of different sources, or that the structure of the source depends on an adjustable control parameter such as pressure or temperature. We repeat the double-diffraction experiment with different source structures, until the interference pattern on the detector indicates that there is a perfect match between the structure of the source and the structure of the target. This may seem to be a simple procedure, however this procedure has a good signal-to-noise ratio for system identification only if the system parameters are well adjusted. Some of the important system parameters are the minimum number of scatterers in the source, the distance between the source and the target, and the distance between the target and the detector. In the following we discuss the adjustment of these and other parameters.

The double-diffraction system. – We consider systems where the dynamics of the field $\mathbf{E}(\mathbf{r}, t)$, at

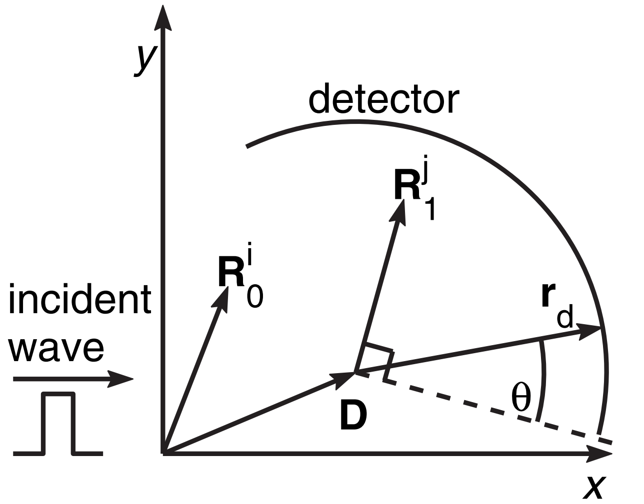

Fig. 1: Schematics of a double-diffraction system. $\mathbf{R}_0^i$ indicates the direction of the source scatterers and $\mathbf{R}_1^j$ indicates the direction of the target scatterers. $\mathbf{D}$ is the displacement from the source scatterers to the target scatterers. θ is the diffraction angle.

position $\mathbf{r}$ and time t is given by a linear wave equation

$$\frac{\partial \mathbf{E}}{\partial t} - c^2\nabla^2\mathbf{E} = \mathbf{0} \qquad (1)$$

where c is the wave speed and ∇^2 is the Laplacian operator in a d-dimensional space, and $d = 1, 2, \ldots$. The setup of the double-diffraction technique is illustrated in fig. 1. The source is a linear arrangement of N_0 scatterers where the distances between the scatterers is an aperiodic sequence. The unit vector $\hat{\mathbf{R}}_0$ indicates the direction of the source. $\mathbf{R}_0^i = R_0^i\hat{\mathbf{R}}_0$ is the position of the i-th source scatterer. The distribution function of the source scatterers is $L_0(\mathbf{r}) = \sum_{i=1}^{N_0} \frac{1}{\delta_s}\Pi(|\mathbf{R}_0^i - \mathbf{r}|/\delta_s)$, where δ_s is the size of the scatterer and Π is the rectangular function. The target is a linear arrangement of scatterers too, where the distances between the scatterers is typically a different aperiodic sequence. The unit vector $\hat{\mathbf{R}}_1$ indicates the direction of the target. $\mathbf{T}^j = \mathbf{D} + \mathbf{R}_1^j$ is the position of the j-th target scatterer, where $\mathbf{R}_1^j = R_1^j\hat{\mathbf{R}}_1$, $\mathbf{D} = D\hat{\mathbf{D}}$, and $\hat{\mathbf{D}}$ is a unit vector. The distribution function of the target scatterers is $L_1(\mathbf{r}) = \sum_{j=1}^{N_1} \frac{1}{\delta_s}\Pi(|\mathbf{D} + \mathbf{R}_1^j - \mathbf{r}|/\delta_s)$. The detector is located on a circle with radius r_d, centered at $\mathbf{D}$. $\mathbf{r}_d = r_d\hat{\mathbf{r}}_d$ is the vector from $\mathbf{D}$ to a location on the detector, where θ is the angle between a normal vector to the direction of the target scatterers and $\mathbf{r}_d$, *i.e.* $\sin\theta = \hat{\mathbf{R}}_1 \cdot \hat{\mathbf{r}}_d$. θ is the diffraction angle. The quasiperiodic structure of the source and the target is constructed with the (P)roject (A)nd (C)ut procedure [17,18] with structural parameters (α_0, β_0) and (α_1, β_0), respectively:

$$R_0^i = \left(i + (\cot\alpha_0 - 1)\left\lfloor \frac{i}{1+\tan\alpha_0} + \beta_0 \right\rfloor\right) a_0 \sin\alpha_0\,, \quad (2)$$

$$R_1^j = \left(j + (\cot\alpha_1 - 1)\left\lfloor \frac{j}{1+\tan\alpha_1} + \beta_1 \right\rfloor\right) a_1 \sin\alpha_1\,, \quad (3)$$

where $i = 1\ldots, N_0$ and $j = 1\ldots, N_1$. N_0, N_1 are the numbers of source scatterers and target scatterers, respectively. $\lfloor\,\rfloor$ is the floor function and β_0 and β_1 are the phases of the floor function. In the following we consider the case where $\beta_0 = \beta_1 = 0$. The parameters a_0 and a_1 adjust the distance between neighboring scatterers. In the source the distance between neighboring scatterers is either $A_0 = a_0\sin\alpha_0$ or $B_0 = a_0\cos\alpha_0$, and $A_1 = a_1\sin\alpha_1$ or $B_1 = a_1\cos\alpha_1$ in the target. Hence $R_0^i = \sum_{k=0}^{i} A_0 + (B_0 - A_0)s_0^k$ and $R_1^j = \sum_{k=0}^{j} A_1 + (B_1 - A_1)s_1^k$ are weighted partial sums of the binary sequences $S_0 = \{s_0^1 s_0^2 \ldots s_0^{N_0-1}\}$ and $S_1 = \{s_1^1 s_1^2 \ldots s_1^{N_1-1}\}$, such as $S_0 = \{00100101\ldots\}$ and $S_1 = \{01000010\ldots\}$. In general, $\alpha_0 \neq \alpha_1$, thus the two sequences S_0 and S_1 are different. The average spacing between two scatterers is $\bar{l}_n = A_n\tau_n/(1+\tau_n) + B_n/(1+\tau_n) = a_n\sqrt{1+\tau_n^2}/(1+\tau_n)$, where $n = 0,\ 1$ and $\tau_n = \cot\alpha_n$. Hence the expectation value of the size of the source is $\bar{R}_0^{N_0} = N_0 a_0\sqrt{1+\tau_0^2}/(1+\tau_0)$ and the expectation value of the size of the target is $\bar{R}_1^{N_1} = N_1 a_1\sqrt{1+\tau_1^2}/(1+\tau_1)$. If a τ-value is the golden mean $\tau_n = (1+\sqrt{5})/2$, then the corresponding sequence S_n is the Fibonacci chain [19]. In our numerical simulations the target scatterers are a Fibonacci chain, *i.e.* $\tau_1 = (1+\sqrt{5})/2$.

$\hat{\mathbf{k}} = (1, 0)$ is the direction of the wave vector of the incident wave. The incident wave is a delta pulse of height E_0 and duration δ, *i.e.* the field of the incident wave is $E_I(\mathbf{r}, t) = E_0\Pi((t - \mathbf{r}\cdot\hat{\mathbf{k}}/c)/\delta)$. We consider systems where $\hat{\mathbf{k}}$, $\hat{\mathbf{R}}_0$, $\hat{\mathbf{R}}_1$, and $\hat{\mathbf{D}}$ are coplanar.

In the numerical experiment we change the structural parameter of the source α_0 systematically and keep the structural parameter of the target α_1 constant. In a system identification experiment the structural parameter of the source is assumed to be known, whereas the structural parameter of the target is unknown. The field diffracted from the source is

$$E_s(\mathbf{r}, t) = \int CE_I(\tilde{\mathbf{r}}, \tilde{t})L_0(\tilde{\mathbf{r}})G(\mathbf{r}, t, \tilde{\mathbf{r}}, \tilde{t})\mathrm{d}\tilde{\mathbf{r}}\mathrm{d}\tilde{t}, \qquad (4)$$

where C is the scattering strength of each scatterer, and $G(\mathbf{r}, t, \tilde{\mathbf{r}}, \tilde{t}) = \delta(\tilde{t} - t - |\mathbf{r} - \tilde{\mathbf{r}}|/c)/|\mathbf{r} - \tilde{\mathbf{r}}|^{d-1}$ is the propagator for eq. (1). If the target is far from the source ($D \gg \bar{R}_0^{N_0}$), and if the size of the scatterers is small ($\delta_s \ll \bar{R}_0^{N_0}/N_0$), E_s is a pulse train of planar waves near the target:

$$\begin{aligned} E_s(\mathbf{r}, t) &\approx \sum_{i=1}^{N_0} \frac{C}{r^{d-1}} E_I\left(0, t - \frac{((\mathbf{r} - \mathbf{R}_0^i)\cdot\mathbf{r}/r + \mathbf{R}_0^i\cdot\hat{\mathbf{k}})}{c}\right) \\ &= \frac{CE_0}{r^{d-1}}\sum_{i=1}^{N_0}\Pi\left(\frac{t}{\delta} - \frac{r - R_0^i(\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} - \hat{\mathbf{R}}_0\cdot\mathbf{r}/r)}{c\delta}\right) \\ &\approx c_1\sum_{i=1}^{N_0}\Pi((r - R_0^i c_3 + c_4)/c_2), \end{aligned} \qquad (5)$$

where $c_1 = CE_0/D^{d-1}$, $c_2 = -c\delta$, $c_3 = \hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} - \hat{\mathbf{R}}_0\cdot\hat{\mathbf{D}}$, $c_4 = ct$, and $r = |\mathbf{r}|$. The space dependence of the distribution function of the source (in the direction of the source) $L_0(r\hat{\mathbf{R}}_0) = \frac{1}{\delta_s}\sum_{i=1}^{N_0}\Pi((|\mathbf{r}| - R_0^i)/\delta_s)$, and the space dependence of the pulse train (in the direction of the target scatterers) $E_s(r\hat{\mathbf{D}})$ is the same, except for the magnitude c_1 and length of the pulses c_2, the change in length of the pulse train by the factor c_3, and a displacement c_4. The distances of the pulses in the pulse train have one of the two values $\tilde{A}_0 = A_0(\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} - \hat{\mathbf{R}}_0\cdot\hat{\mathbf{D}})$ and $\tilde{B}_0 = B_0(\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} - \hat{\mathbf{R}}_0\cdot\hat{\mathbf{D}})$. The pulses may overlap if their separation is less than the pulse length, *i.e.* $\max\{A_0, B_0\} < \delta$, or $\max\{\sin\alpha_0, \cos\alpha_0\}|(\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} - \hat{\mathbf{R}}_0\cdot\hat{\mathbf{D}})| < \delta/a_0$.

Time dependence of the field at the detector. – If we assume that a screen prevents incident beam and the quasiperiodic pulse train from reaching the detector, the field at the detector is the sum of the contributions from all the target scatterers

$$E_d(\mathbf{r}_d, t) = \int C E_s(\tilde{\mathbf{r}}, \tilde{t}) L_r(\tilde{\mathbf{r}}) G(\mathbf{D} + \mathbf{r}_d, t, \tilde{\mathbf{r}}, \tilde{t})\mathrm{d}\tilde{\mathbf{r}}\mathrm{d}\tilde{t}$$
$$\approx \sum_{j=1}^{N_1} \frac{C}{|\mathbf{r}_{-}\mathbf{R}_1^j|} E_s\left(\mathbf{R}_1^j + \mathbf{D}, t - \frac{|\mathbf{r}_d - \mathbf{R}_1^j|}{c}\right) \quad (6)$$

if the size of the target scatterers is small. Since $\mathbf{r}_d$ is a function of the diffraction angle θ, the field at the detector is a function of the diffraction angle, *i.e.* $E_d(\mathbf{r}_d, t) = E_d(\theta, t)$. We express the field at the detector in terms of the incident wave at the origin and the diffraction angle:

$$E_d(\theta, t) = \sum_{i,j=1}^{N_0,N_1} \frac{C^2}{|\mathbf{r}_d(\theta) - \mathbf{R}_1^j|^{d-1}|\mathbf{R}_1^j + \mathbf{D} - \mathbf{R}_0^i|^{d-1}}$$
$$\times E_I\left(0, t - \frac{|\mathbf{r}_d(\theta) - \mathbf{R}_1^j| + |\mathbf{R}_1^j + \mathbf{D} - \mathbf{R}_0^i| + \mathbf{R}_0^i\cdot\hat{\mathbf{k}}}{c}\right)$$
$$= \sum_{i,j=1}^{N_0,N_1} \frac{C^2 E_0}{|\mathbf{r}_d(\theta) - \mathbf{R}_1^j|^{d-1}|\mathbf{R}_1 + \mathbf{D} - \mathbf{R}_0|^{d-1}}$$
$$\times \Pi\left(\frac{t}{\delta} - \frac{|\mathbf{r}_d(\theta) - \mathbf{R}_1^j| + |\mathbf{R}_1^j + \mathbf{D} - \mathbf{R}_0^i| + \mathbf{R}_0^i\cdot\hat{\mathbf{k}}}{c\delta}\right)$$
$$\approx \sum_{i,j=1}^{N_0,N_1} \frac{C^2 E_0}{(r_d D)^{d-1}}$$
$$\times \Pi\left(\frac{t}{\delta} - \frac{|\mathbf{r}_d(\theta) - \mathbf{R}_1^j| + |\mathbf{R}_1^j + \mathbf{D} - \mathbf{R}_0^i| + \mathbf{R}_0^i\cdot\hat{\mathbf{k}}}{c\delta}\right). \quad (7)$$

Figure 2 shows the typical time dependence of the intensity of the field $I(t) = E_d^2(\theta, t)$ at the detector for $d = 2$, where $\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} = 0$, $\hat{\mathbf{R}}_0 = \hat{\mathbf{D}}$, and $\hat{\mathbf{R}}_1 = -\hat{\mathbf{k}}$. The distance between two scatterers is $D = 10^5$. The distance from the target detector to the screen is $r = 10^4$. The wave speed is $c = 1$, the amplitude of the original delta pulse $E_0 = 100$, and the width of the delta pulse $\delta = 0.02$. The detector placed at $\theta = \pi/2$ and the structural parameters of the source and target scatterers are $\tau_0 = \tau_1 = (1 + \sqrt{5})/2$ and $a_0 = a_1 = 1$. The scattering intensity is $C = 1$.

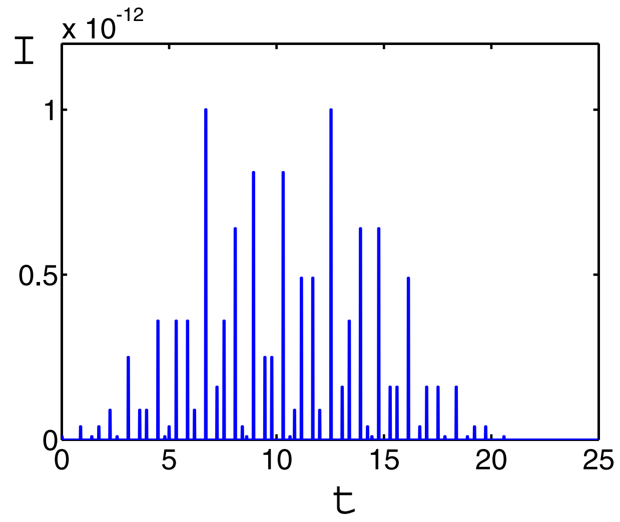

Fig. 2: A typical time dependence of the intensity of the field I at the detector.

Diffraction patterns. – If the sequence of target S_1 is a subsequence of the source S_0, then constructive interference from all N_1 target scatterers occurs at the diffraction angle

$$\theta_{max} = \arcsin\left(\hat{\mathbf{R}}_1\cdot\hat{\mathbf{D}} + (\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} - \hat{\mathbf{R}}_0\cdot\hat{\mathbf{D}})\frac{a_0}{a_1}\right). \quad (8)$$

Figure 3 shows the maximum intensity $I_{max} = \max_t(E_d(\theta, t)^2)$ *vs.* the diffraction angle θ for the system described in fig. 2, except that $a_0 = 0.9$. The diffraction pattern has a pronounced peak at the diffraction angle $\theta_{max} = \arcsin(a_0) \approx 1.12$. If there is constructive interference from all target scatterers the maximum intensity at the detector is

$$I_{max} \approx \left(N_1 \frac{C^2 E_0}{(rD)^{d-1}}\right)^2. \quad (9)$$

The numerical value in fig. 3 agrees well with the theoretical value $I_{max} = 10^{-12}$.

For double-diffraction systems $\hat{\mathbf{R}}_0\cdot\hat{\mathbf{k}} = 0$, $\hat{\mathbf{R}}_0 = \hat{\mathbf{D}}$, and $\hat{\mathbf{R}}_1 = -\hat{\mathbf{k}}$ and $\theta = \theta_{max}$ eq. (7) simplifies to

$$E_d = \frac{C^2 E_0}{(r_d D)^{d-1}} \times \sum_{i,j=1}^{N_0,N_1} \Pi\left(\frac{t}{\delta} - \frac{r_d + R_1^j + \sqrt{(R_1^j)^2 + (D - R_0^i)^2}}{c\delta}\right)$$
$$\approx \frac{C^2 E_0}{(r_d D)^{d-1}} \sum_{i,j=1}^{N_0,N_1} \Pi\left(\frac{t}{\delta} - \frac{r_d + D + R_1^j - R_0^i + \frac{(R_i^i)^2}{2D}}{c\delta}\right)$$
$$= \mathcal{A}(r_d, D, d) \sum_{i,j=1}^{N_0,N_1} \Pi\left(\frac{t}{\delta} - \frac{\mathcal{L}(r_d, R_0^i, R_1^j, D)}{c\delta}\right), \quad (10)$$

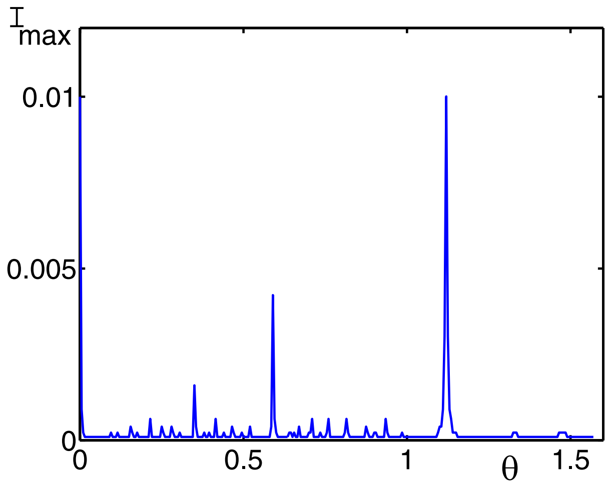

Fig. 3: The maximum intensity *vs.* the diffraction angle for a double-diffraction system, where both the source scatterers and the target scatterers are Fibonacci chains. The number of source scatterers $N_0 = 20$, and the number of target scatterers is $N_1 = 10$. The scaling parameters of the scatterers are $a_0 = 0.9$ and $a_1 = 1$. The location of the diffraction peak is close to the theoretical value $\theta_{max} = \arcsin(a_0/a_1) \approx 1.12$. The height of the main diffraction peak is close to the theoretical value $I_{max} = 0.01 \times 10^{-10}$.

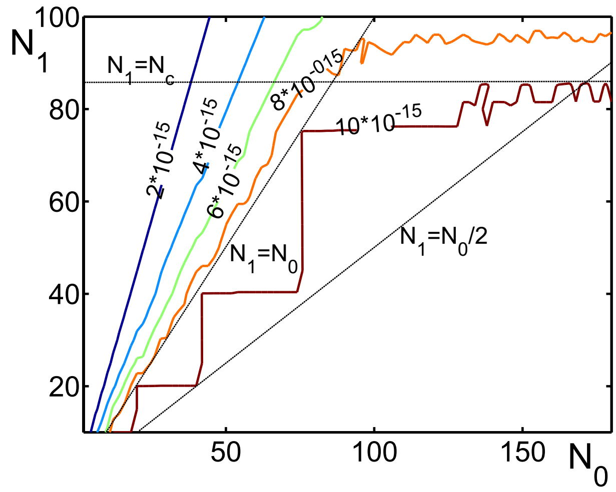

Fig. 4: The contour plot of the relative intensity I_{max}/N_1^2 *vs.* N_0 and N_1.

Table 1: Comparison between theoretical estimates and simulation of N_c.

δ	N_c estimated	N_c simulated
0.01	61.55	62 ± 2
0.02	87.05	88 ± 2
0.03	106.61	108 ± 2

where $\mathcal{A}(r_d, D, d) \equiv C^2 E_0/(r_d D)^{d-1}$ is the amplitude, and $\mathcal{L}(r_d, R_0^i, R_1^j, D) \equiv r_d + D + R_1^j - R_0^i + (R_i^i)^2/(2D)$ is a phase shift. r_d and D are constant for all terms of the sum. There is constructive interference from all N_1 target scatterers, if the quadratic term in the phase shift $\mathcal{L}$ is negligible small and if there is an i-value where the expression $a_1 R_0^{i+j} - a_0 R_1^j = a_1 R_0^i$ for $j = 1, 2, \ldots, N_1$, *i.e.* if the sequence S_1 is a subsequence of S_0.

Limitations of the double-diffraction system. – Equation (9) suggests that the relative intensity I_{max}/N_1^2 is independent of N_1 and N_0. Figure 4 is a contour plot of the relative intensity *vs.* N_0 and N_1, where the parameters are the same as in fig. 2. It shows that the relative intensity is equal to the theoretical value given by eq. (9), $I_{max}/N_1^2 = 10^{-14}$ if the number of target scatterers N_1 is less than the value N_c, and less than half the number of source scatterers, *i.e.* $N_1 < \min\{N_c, N_0/2\}$. If $\min\{N_c, N_0/2\} < N_1 < \min\{N_c, N_0\}$ the relative intensity is sometimes equal to the theoretical value and sometimes less. For $\min\{N_c, N_0\} < N_1$ the relative intensity is always less than the theoretical value. If $N_0 < N_1$ then the sequence S_0 is shorter than the sequence S_1, and therefore S_1 cannot be a subsequence of S_0. Hence there is no constructive interference from all N_1 scatterers. If $N_0 > 2 * N_1$, S_1 is always a subsequence of S_0, since the recurrence time for PAC sequences is twice the length of the sequence [17], and therefore there is constructive interference from all N_1 target scatterers. In the intermediate region constructive interference may or may not occur.

Figure 4 also shows that constructive interference from all N_1 scatterers does not occur if N_1 exceeds the value N_c, no matter how large N_0. This is due to the quadratic term in the phase shift. If the quadratic term for a scatterer exceeds the pulse width, *i.e.* $(\bar{R}_1^{N_c})^2/(2D) > c\delta$, full constructive interference from all N_1 target scatterers will no longer occur. Therefore, the value N_1 can be estimated with

$$\bar{R}_1^{N_c} \approx \sqrt{2Dc\,\delta}. \qquad (11)$$

With $\bar{R}_1^{N_1} = N_1 a_1 \sqrt{1+\tau_1^2}/(1+\tau_1)$ we obtain

$$N_c \approx \sqrt{2Dc\,\delta}\,\frac{1+\tau_1}{a_1\sqrt{1+\tau_1^2}}. \qquad (12)$$

Table 1 shows a comparison between numerical estimates and the theoretical value for several N_c values.

System identification with double diffraction. – The main peak in the diffraction pattern can be used to identify the structure of the target scatterers. Figure 5 shows the height of the main diffraction peak *vs.* the structural parameter of the source scatterers α_0. The number of scatters is $N_0 = 30$ and $N_1 = 15$. The other parameters are the same as in fig. 2. Within the parameter range $0.540 < \alpha_0 < 0.566$ the intensity is constant and the numerical value is very close the theoretical value given by eq. (9). Hence the numerical estimate of the structural parameter of the target is $\alpha_1 = 0.553 \pm 0.14$.

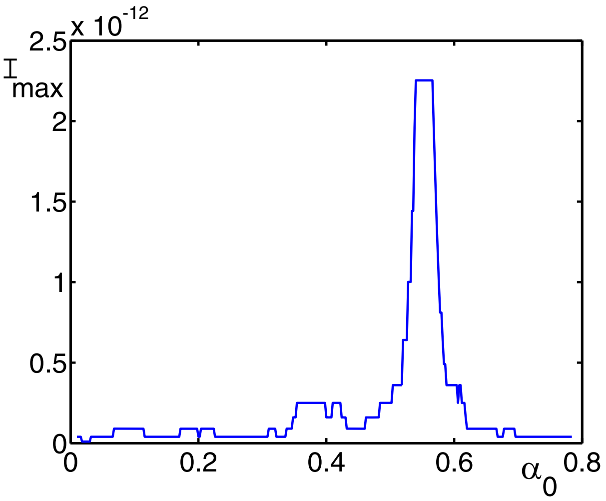

Fig. 5: The intensity of the main peak $I_{max}(\theta_{max})$ *vs.* the structural parameter of the source α_0.

The actual parameter of the source scatterers is $\alpha_1 = \arctan(2/(1+\sqrt{5})) \approx 0.5536$, which is consistent with the numerical estimate.

Conclusion. – We have demonstrated that double diffraction can be used to detect the structure of a quasiperiodic set of scatterers (see fig. 5). We estimate N_c, the maximum number of the number of target scatterers which contribute to constructive interference, in terms of the width of the original pulse and the distance between two set of scatterers and the structural parameter of the target τ_1 (see eq. (11)). We show that the number of target scatterers which contribute to the constructive interference is $N = \min\{N_c, N_1\}$, if the source has at least $2N$ scatterers (see fig. 4). The width of the resonance curve (see fig. 4) is only 5%. This means that the structural parameter of the source and the target have to be close to see any resonance effect at all, however it also means that the structural parameter of the target can be determined with about good accuracy. The double-diffraction method can also be used to differentiate between targets with and without defects. Temperature-induced defects in quasiperiodic sequences, called phasons [20,21], alter the quasiperiodic sequence and reduce the height of the resonance curve in fig. 4. In addition, this double-diffraction technique can be applied to determine the structure and orientation of Fibonacci multilayers. In a typical material with quasiperiodic multilayers, the thickness of each layer is on the order of $\bar{l} = 100$ nm, and the number of layers is on the order of 100 [22]. If we use a laser pulse to probe the structure, the length of the pulse has to be at the similar scale, or $c\,\delta \approx 10^{-7}$ m. Therefore, the duration of the pulse δ is at the 100–1000 attosecond range. Attosecond pulses in this range have been observed experimentally in 2001 [23,24]. If the distance between source scatterers and the target scatterers $D = 10$ micron, the critical number of the target scatterers $N_c \approx 140$ (see eq. (12)), which is also within the experimental range. Therefore, it should be possible to determine the structure and orientation of quasiperiodic multilayers in double-diffraction experiments with the existing technology.

* * *

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